I Appendix A SCHOLZ (attenuation according to position of switch)  $RI = \frac{\alpha RO \cdot RI}{\alpha RO + RI}$   $R2 = \frac{(1-\alpha)RO \cdot ZL}{(1-\alpha)RO \cdot ZL}$  $U_{L} = \frac{\hat{R}_{2}}{\hat{R}_{1} + \hat{R}_{2}} U_{0} = \frac{1}{1 + \frac{\hat{R}_{1}}{\hat{R}_{2}}} U_{0} = \frac{1}{1 + \left(\frac{\alpha}{1 - \alpha}\right) \frac{R_{1}}{2} \cdot \frac{(r_{\alpha})R_{0} + Z_{L}}{r_{1} + \alpha}}$ (If assumed that ZL < RO (SCHOLZ requires RI+ZL < RO))  $U_{L} = \frac{1}{1 + \left(\frac{\alpha}{1-\alpha}\right) \frac{R1}{2!} \cdot \left(\frac{1-\alpha}{RO + R1}\right) V_{O}} \approx \frac{1}{1 + \alpha \frac{RO}{2L}}$ Because ZL is frequency-dependent (Rz-iwL) the Voltage UL is not in constant relation to Vo

Appendix A  $(1-\alpha)ZO^{\frac{3}{3}}$   $\frac{3}{3}ZL$   $(1-\alpha)ZO^{\frac{3}{3}}$   $\frac{3}{3}ZL$   $(1-\alpha)ZO^{\frac{3}{3}}$   $\frac{3}{3}ZL$  $U_{L} = \frac{1}{1 + \frac{21}{22}} = \frac{1}{1 + \left(\frac{\alpha}{1 - \alpha}\right) \cdot \frac{(1 - \alpha) 20 + 2L}{2L}} \quad V_{0}$ For law frequencies  $U_{L} \approx \frac{1}{1+(\frac{\alpha}{1-\alpha})} U_{0}$ (zl << zo = -iwlo) UL = 1+ (x/1-x).(1-x) Lo 20 (ωLo) frequency Grequence Frequency-dependent in first

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Appendix A  $\frac{1}{1+\left(\frac{\alpha}{1-\alpha}\right)\frac{R_1}{ZL}} \cdot \frac{(1-\alpha)Z_0+Z_L}{\alpha Z_0+R_1} \cup 0$ See is in approximate proportion to ZL => Z0=BZL Larger than Zo => & Zo+R, & R, no frequency-dependence in first order